

ACES CATS

Calculation of ADSS Tension and Sag

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Registered Continuing Education Program PURPOSE STATEMENT / COURSE DESCRIPTION

- ADSS ENGINEERING 102 Sag and Tension will teach you how to obtain the sag and tension data that you need for your project.
- We will explain and illustrate three methods of obtaining sag and tension data as per industry practice today:
 - 1. Using tabulated data supplied by cable manufacturers,
 - 2. Generating data using ACES CATS, and
 - 3. Using PLS-CADD to perform sag and tension calculations.
- Then we will discover how the preceding is technically incorrect, but why it is nevertheless helpful. This will lead us to consider the difference between mechanically independent versus mechanically coupled spans. From this, we will learn when today's practice is appropriate, and when the ruling span concept should be applied and sag and tension data obtained from computer programs such as PLS-CADD.
- Along the way, we will explain the meaning and importance of a cable's "Maximum Rated Design Tension" (MRDT), and how it should be used in sag and tension calculations. And, we will do likewise for Zero Fiber Strain Margin (ZFSM).

Registered Continuing Education Program LEARNING OBJECTIVES

After this class you will be able to:

- Be able to obtain basic sag and tension data for your ADSS cable using these sources:
 - 1. Tabulated data supplied by cable manufacturers,
 - 2. Self-generated data using ACES CATS (and be able to use it), and
 - 3. Computer programs, in particular PLS-CADD.
- Explain the meaning and importance of a cable's Maximum Rated Design Tension (MRDT), Zero Fiber Strain Margin (ZFSM) and how these should be incorporating into sag and tension data.
- State the implicit assumptions of industry practice for ADSS sag and tension data.
- Explain the difference between mechanically independent and mechanically coupled spans.
- Know when it is more appropriate to apply the ruling span concept and use PLS-CADD or other computer software to generate sag and tension data for ADSS.

Incab University "School of Excellence in Fiber Optics" curriculum

Webinar Rules

- Introduction and sound check
- Presentation: 45 min
- Use chat for questions during presentation
- Q&A (NB! Technical questions only): 15 min
- Let's start!





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 Let's begin our study of ADSS sag and tension with three observations...

Sag and tension observation 1

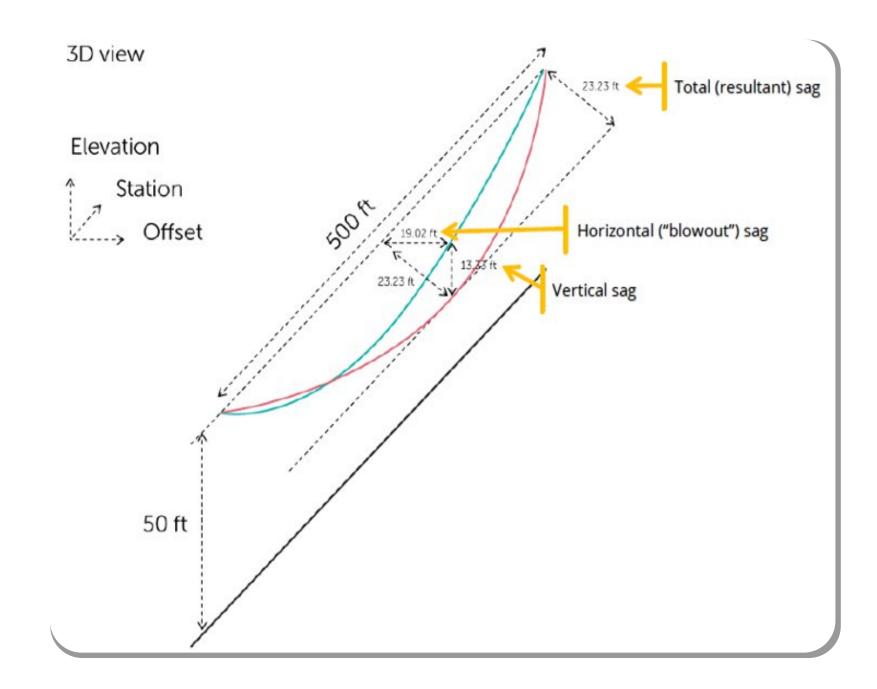
- If someone tells you:
 "Snow and ice don't accumulate on ADSS in the field"
- Please show them this picture
- It is a myth that ice does not accumulate on ADSS!
- Vertical sag under ice loading can exceed ground clearance, and consequently, it must be checked!



Note how large the sag is too

ADSS sag and tension data Sag and tension observation 2

- Wind conditions are especially important for ADSS
- ADSS is light and elastic
- Consequently, horizontal blowout during wind loading can be significant and must be checked!



ADSS sag and tension data Sag and tension observation 3

- Because ADSS is very elastic, strength is needed to control fiber strain
 - Fiber strain can lead to optical failure over time

OK. This prompts the question: What is fiber strain, and why is it important?

Side tour: Fiber Strain

What is fiber strain, and why is it important?

- Fiber strain is tension on the fiber
- Optical fiber is strong, but it is glass, so it is brittle
 - * Thus, keeping tension off the fiber is a good idea

 enhances reliability
 - "No strain, no problems"
 - * Fiber is especially vulnerable to adverse effects from cyclic loading
- Fiber Strain Margin is the difference between the tension on the cable and the tension on the fiber
 - * The "Zero Fiber Strain Margin" (ZFSM) is the point at which the optical fibers begin to experience tension
 - * General Guideline: The higher the ZFSM, the better

Let's connect the three observations

- In order to properly check clearances, sag and tension calculations for ADSS need to factor in ice and wind loading
- Note: Industry practice has been to have "installation" or "everyday" sag = 1% or 1.5% of span
 - More recently have seen 0.75% and even 0.5% (risky in my opinion)

And...

Let's connect the three observations, cont'd

- Fiber strain should be minimized (or zero fiber strain margin maximized)
 - "Best Practice" is zero fiber strain through "MRDT" (defined on next slide)
 - This is Incab's design standard, but sometimes not practical
 - Acceptable alternates (with increasing risk):
 - Zero fiber strain at nominal (unloaded) tension ("everyday")
 - Limited fiber strain at maximum (loaded) tension (MRDT)
 - * Good, ≤ 0.2%
 - Conservative limit derived from Corning research
 - * Not too bad, ≤ 0.3%
 - Acceptable for today's fiber, but does have some risk
 - * Risky, ≤ 0.4% Greater than this is just plain crazy!

All cable suppliers have a design policy on fiber strain! (Though not always clearly disclosed)

MAXIMUM RATED DESIGN TENSION (MRDT)

- MRDT (= MRCL "maximum rated cable load") is an especially important cable specification!
 - MRDT = The tension the cable should <u>NEVER</u>, <u>EVER</u> exceed under <u>any</u> loading condition!
 - MRDT (MRCL) is NOT the same as Rated Breaking Strength (RBS)!
 - Typically, MRDT (MRCL) is 50 65% of RBS

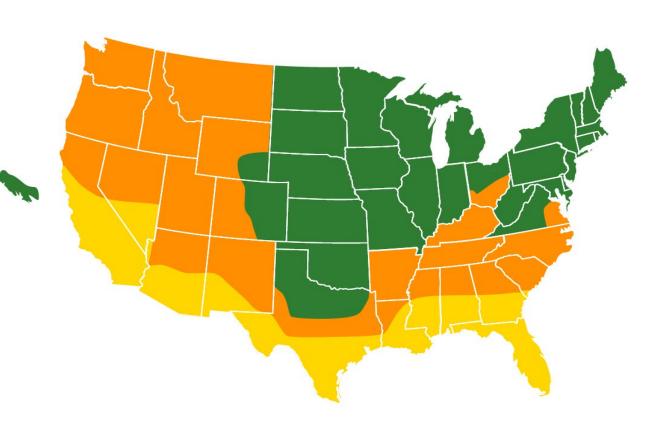
DATA GENERATION IN 3 EASY STEPS!

- Step 1 = Review your loading criteria
- Step 2 = Get the cable specifications
- Step 3 = Get or generate the data

Let's explore each step...

STEP 1: REVIEW YOUR LOADING CRITERIA

- Determine your base loading criteria
 - * NESC Rule 250B loading zone
 - * Alternate for your state or country
- Do you have "extreme ice" or "concurrent wind and ice" conditions?
 - * NESC Rule 250C and D
 - * Additional criteria for your state or country
- Criteria unique to your utility or project?
 - * Tension limits?
 - * Sag limits?



STEP 2: GET THE CABLE SPECIFICATIONS

- Basic cable specifications are needed to generate sag and tension data:
 - 1. Outside diameter (inches or mm)
 - 2. Unit weight (lb/ft or kg/km)
 - 3. Maximum Rated Design Tension (MRDT)
 - 4. Cable modulus (Which to use? We'll come back to that.)
 - 5. Linear expansion coefficient
 - 6. Strain limit. Ideally the "zero fiber strain margin" (ZFSM)
- You'll find these on the cable datasheet or ask the cable manufacturer
- P Let's look at typical cable datasheets from various suppliers and see how they present this information....

STEP 2: GETTING THE SPECIFICATIONS -

T Aramid DJ-144U (12x12)-13kN

	Design details			
	Fiber count		144	
	Number of loose tubes		12	
	Fibers per loose tube		12	
	Number of fillers		-	
	Loose tube diameter	mm (in)	3.0 (0.118)	
	Inner jacket thickness	mm (in)	0.7 (0.028)	
	Outer jacket thickness	mm (in)	1.6 (0.063)	
1	Cable diameter ± 0.2 (0.008)	mm (in)	20.3 (0.799)	
2	Cable weight	kg/km (lb/ft)	298.1 (0.2)	
3	Maximum rated design tension	kN (lb)	13.0 (2923)	
6	Zero fiber strain margin	kN (lb)	10.6 (2383)	
	Stringing tension (STT)	kN (lb)	3.25 (731)	
	Rated breaking strength (RBS)	kN (lb)	20.0 (4497)	
4	Modulus of elasticity, initial	kN/ mm² (ksi)	3.87 (561)	Note: We will discuss modulus leter
	Modulus of elasticity, final	kN/mm² (ksi)	4.17 (606)	Note: We will discuss modulus later
	10-year modulus of elasticity, creep	kN/mm² (ksi)	3.01 (438)	
	Cable cross-sectional area	mm² (in²)	322.4 (0.5)	
5	Coefficient of thermal expansion, 10 ⁻⁶	1/°C (1/°F)	15.52 (8.62)	

STEP 2: GETTING THE SPECIFICATIONS –

P7 R 3/1 SPAN PKP 1581LB (12F/T) TR (#ADLT1581-12-HB-072)

Cable Specifications:

Maximum Rated Cable Load: =	MRDT 1581	lb	
Cable Diameter:	0.508	in	
Cross Sectional Area:	0.203	in ²	
2 Cable Weight:	0.099	lb/ft	
Ultimate Tensile Strength:	3954	lb	
Sheath Configuration:	Dual Jacket		
Outer Jacket Type:	Track Resistant		

Additional Design Information for PLS-CADD & SAG10:

Initial Modulus of Elasticity:

10-year Modulus of Elasticity:

Final Modulus of Elasticity:

5 Coefficient of Thermal Expansion:

918 kpsi
843 kpsi
918 kpsi (See note 2)
1.80E-05 1/°F

Maximum Tension At Maximum Span:

6 Long Term: (See note Short Term: 1)

638 lb ≤ ZFSM 1575 lb ≤ MRDT = OK

Note 1: Fiber Strain Margin 6 is not directly shown, but is factored into their sag & tension data (will see this later)

Note 2: Initial = Final = Not really. This is a simplification that's OK in the distribution world...More on this later

STEP 2: GETTING THE SPECIFICATIONS – OFS

AT-XXX27D6-048-TMEE-JX

Fension @ Maximum Span for 1 % Installation	n Sag)
Short Term Used as MRDT	1815 kg	4002 lb
6 Long Term (See note)	898 kg	1979 lb
Specifications:		100000000000000000000000000000000000000
Maximum Span	389 m	1276 ft
Cable Weight	0.185 kg/m	0.124 lb/ft
Cable Diameter	15.2 mm	0.599 in
Installation Temp	20 C	68 F
4 Cable Modulus	1002.1 kg/mm^2	1425.6 kpsi
5 Linear Expansion Coefficient	0.00000451 1/C	0.00000251 1/F
Estimated Break Load	3283 kg	7240 lb

Note 6 Fiber Strain Margin is not directly shown. The "Long Term" tension is used as the maximum "everyday" (no ice, no wind) tension, but this tells you nothing about the fiber strain or ZFSM

STEP 2: GETTING THE SPECIFICATIONS – AFL

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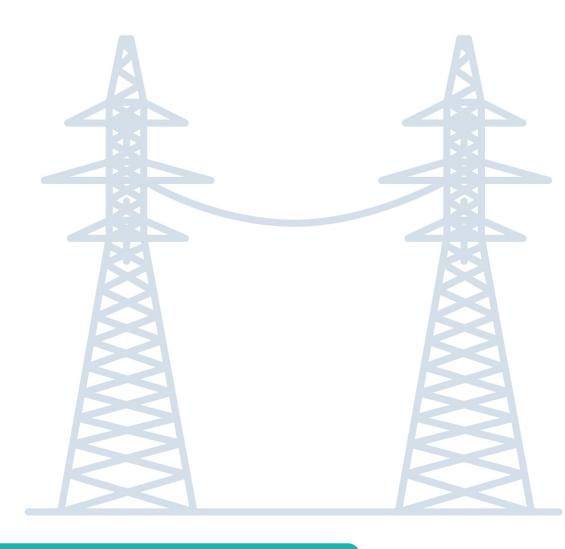
Physical / Mechanical / Elec	trical Characteristic	Metric	English
1 Approximate Cable Diamete	er	12.7 mm	0.500 in
Approximate Cable Weight		123 kg/km	0.083 lbs/ft
Approximate Cable Breaking	ng Strength	564 kg	1,244 lbs
Minimum Bending Radius	Static	127 mm	5 in
	Dynamic	256 mm	12 in
3 — Maximum Rated Cable Loa	d (MRCL) = MRDT	285 kg	628 lbs
Coefficient of Linear Expan	sion	3.64E-05 1/°C	2.02E-05 1/°F
4 Cable Modulus	Initial	2.00 kN/mm^2	290.7 kpsi
	10 Year	1.67 kN/mm^2	242.3 kpsi
	Final	2.16 kN/mm ²	313.5 kpsi

⁶ Fiber Strain Margin - Not provided by this supplier, nor an "everyday" or long-term limit. Must ask.

ADSS sag and tension

STEP 3: GETTING SAG AND TENSION DATA

- Three sources
 - Traditionally: Manufacturer-provided tables
 - Generally limited to standard NESC loading conditions
 - Ask cable supplier if you need other conditions
- ACES CATS A new, fun, and useful way to generate the data that you need!
 - Can be used for any supplier's cable!
- Generate your own data using Power Line[®] Systems PLS-CADD or Southwire[™] Sag10[®]
 - Will only consider PLS-CADD today

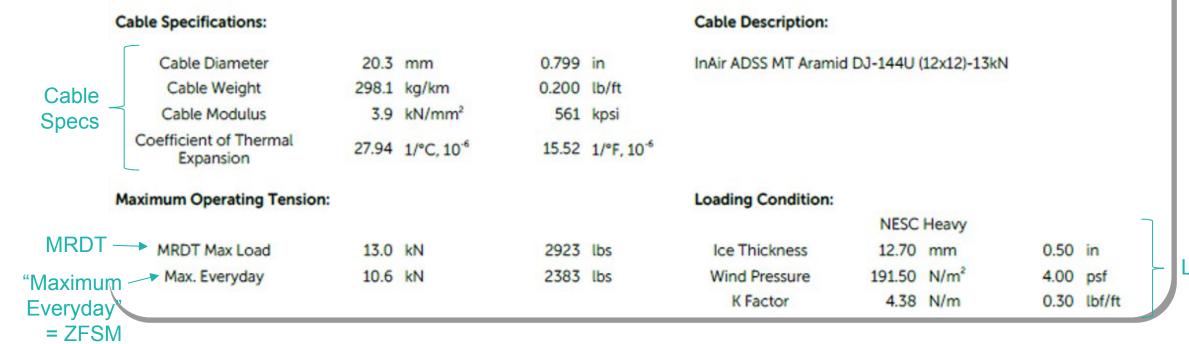


Let's look at each source, starting with data tables from the same four suppliers

DATA TABLES – INCAB

ACES CATS | Advanced Cable Engineering System for Calculation of ADSS Tensions and Sags

ADSS Sags And Tensions Data



Loading Conditions

DATA TABLES – INCAB

Nomi	nal/No Loading. Instal	llation Temp	erature 68 h
Span (ft)	Sag (ft)	Sag (%)	Tension (lb)
50	0.75	1.5	83
100	1.50	1.5	167
150	2.25	1.5	250
200	3.00	1.5	334
250	3.75	1.5	417
300	4.50	1.5	501
350	5.25	1.5	584
400	6.00	1.5	668
450	6.75	1.5	751
500	7.50	1.5	835
550	8.25	1.5	918
600	9.00	1.5	1002
650	9.75	1.5	1085
700	10.50	1.5	1168
720	10.80	1.5	1202

Sag (ft)	% Span (%)	H Sag (ft)	V Sag (ft)	Tension (lb)
0.94	1.9	0.48	0.81	493
2.43	2.4	1.24	2.09	758
4.21	2.8	2.14	3.62	987
6.17	3.1	3.15	5.31	1196
8.29	3.3	4.23	7.13	1390
10.54	3.5	5.38	9.07	1575
12.90	3.7	6.58	11.10	1752
15.36	3.8	7.83	13.21	1922
17.90	4	9.13	15.40	2088
20.52	4.1	10.46	17.65	2248
23.21	4.2	11.83	19.96	2405
25.96	4.3	13.24	22.33	2558
28.78	4.4	14.68	24.76	2708
31.65	4.5	16.14	27.23	2856
32.82	4.6	16.74	28.23	2914

At Loading Condition, Temperature -4 F°

"Sag" is total.

"H Sag" = horizontal component to check blowout

"V Sag" = vertical component to check ground clearance

Data for "Everyday" condition (no wind, no ice)

Data for loaded condition

DATA TABLES – PRYSMIAN

ADSS SAG AND TENSION PROPERTIES

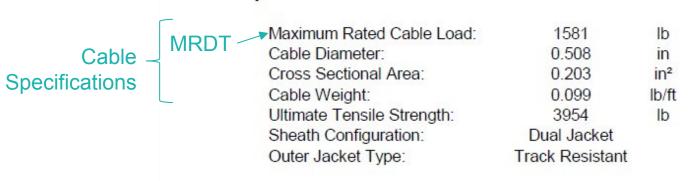
Requirements of:

Fiber Count:	72	Fibers
Maximum Span:	775	ft
Installation Sag:	1.5	%
Installation Temperature:	60	°F
Fiber Strain:	SafeStrain	•

Customer

= Fiber strain = 0 at "everyday" and ≤ 0.2% (?) at MRDT. Ask to confirm.

Cable Specifications:





Loading Conditions: NESC Medium

	Ice Thickness:	0.25	in	
Loading Conditions -	Wind Pressure:	4.0	psf	
Loading Conditions	Temperature:	15	°F	
	Safety Factor:	0.20	lb/ft	
	Maximum Space Potential:	25.0	kV	Low Pollution per IEEE 1222-2011
	Maximum Space Potential	15.0	kV	High Pollution per IEEE 1222-2011

Cable Description: 72F SM ADSS LONG SPAN PKP 1581LB (12F/T) TR
Part Number: ADLT1581-12-HB-072

For comparison.

"ZeroStrain" = Fiber strain = 0 at "everyday" and 0 at MRDT

DATA TABLES – PRYSMIAN

Installation

Span		Installation Sag	
ft	ft	% Span	lb
77.5	1.2	1.5%	64
155.0	2.3	1.5%	128
232.5	3.5	1.5%	191
310.0	4.7	1.5%	255
387.5	5.8	1.5%	319
465.0	7.0	1.5%	383
542.5	8.1	1.5%	447
620.0	9.3	1.5%	510
697.5	10.5	1.5%	574
775.0	11.6	1.5%	638

Data for "Everyday" condition (no wind, no ice)

Maximum Loading Conditions

Span ft	Loaded Vert. Sag ft	Loaded Horiz. Sag ft	Maximum Tension Ib	Cable Angle Degrees	No Wind Vert. Sag ft
77.5	1.1	1.1	317	45	1.5
155.0	2.8	2.9	505	45	3.6
232.5	4.8	4.9	668	45	6.2
310.0	7.1	7.1	817	45	9.0
387.5	9.4	9.5	956	45	12.0
465.0	11.9	12.0	1089	45	15.2
542.5	14.6	14.6	1216	45	18.5
620.0	17.3	17.4	1339	45	22.0
697.5	20.1	20.2	1459	45	25.5
775.0	23.0	23.1	1575	45	29.2

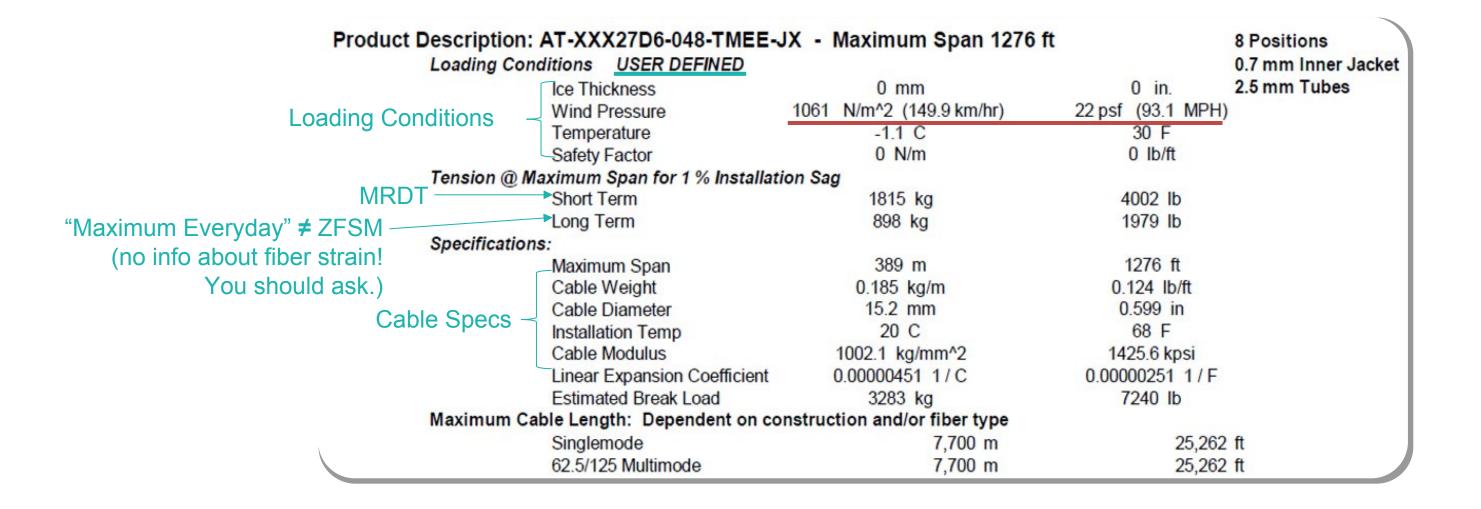
Notice: "Ice Only" vertical sag

Data for loaded condition

"Horiz. Sag" = horizontal sag to check blowout

"Vert. Sag" = vertical sag to check ground clearance

Sag and tension data generation DATA TABLES – OFS



DATA TABLES – OFS

Data for "Everyday" condition (no wind, no ice)

Data under loaded conditions

"H Sag" = horizontal sag to check blowout

"V Sag" = vertical sag to check ground clearance

No Loading	@ Install Tem	perature 68 F	
Span	Sag	Install Sag	Tension
ft	ft	%	lb
100	1.0	1.00	155
200	2.0	1.00	310
300	3.0	1.00	465
400	4.0	1.00	620
500	5.0	1.00	775
600	6.0	1.00	930
700	7.0	1.00	1085
800	8.0	1.00	1241
900	9.0	1.00	1396
1000	10.0	1.00	1551
1100	11.0	1.00	1706
1200	12.0	1.00	1861
1276	12.8	1.00	1979

	All L	oading Conditions	@ Temperature 30 F	
Vertical Sag	Tension	Vertical Sag	Horizontal Sag	Angle
% of Span	lb	ft	ft	Deg
0.2	618	0.2	2.2	84
0.3	1027	0.6	5.4	84
0.3	1378	1.0	9.0	84
0.4	1699	1.5	13.0	84
0.4	2001	1.9	17.3	84
0.4	2286	2.4	21.8	84
0.4	2560	2.9	26.5	84
0.4	2826	3.5	31.3	84
0.4	3084	4.0	36.3	84
0.5	3335	4.6	41.5 Notice	84
0.5	3581	5.2	46.7 how	84
0.5	3822	5.8	52.1 / much	84
0.5	4002	6.3	56.3 blowou	0.4

DATA TABLES – AFL

Tel: 1 800 235 3423 Fax: 1864 433 5560

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	Physical / Mechanical / Electrical Cha	aracteristic Metric	English
	Approximate Cable Diameter	12.7 mm	0.500 in
	Approximate Cable Weight	123 kg/km	0.083 lbs/ft
	Approximate Cable Breaking Strengt	h 564 kg	1,244 lbs
	Minimum Bending Radius Static	127 mm	5 in
Cable Specs	Dynamic	256 mm	12 in
MRDT	Maximum Rated Cable Load (MRCL	285 kg	628 lbs
	Coefficient of Linear Expansion	3.64E-05 1/°C	2.02E-05 1/°F
	Cable Modulus Initial	2.00 kN/mm^2	290.7 kpsi
	10 Year	1.67 kN/mm^2	242.3 kpsi
	Final	2.16 kN/mm ²	313.5 kpsi

Note: Neither "Maximum Everyday" nor ZFSM/fiber strain info shown. You should ask.

DATA TABLES – AFL

	Span Length (ft)	400	Note: Jus	st for one s	pan leng	jth (which	n allows th	em to sho	w multiple	e loading co	nditions)
		Add'I Input Data		a	Resultant Data						
5		Wind	Radial Ice	Load	Vert.	Horiz.	Vector	Vert.	Horiz	Vector	Tension
Data for	Condition	(mi/hr)	(inches)	(lbs/ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(lbs)
"Everyday" condition (no	Installation				4.0			4.00		4.0	415
wind, no ice)	Ice Alone										
	Wind Alone										
Loading Conditions —	Ice and Wind										
	NESC Light	60.0		0.1				3.09	14.3	14.6	605
	Other										
Standard NESC / CSA condition based on Ice Density of 57 lbs/ft³											

"Horiz." = horizontal sag to check blowout

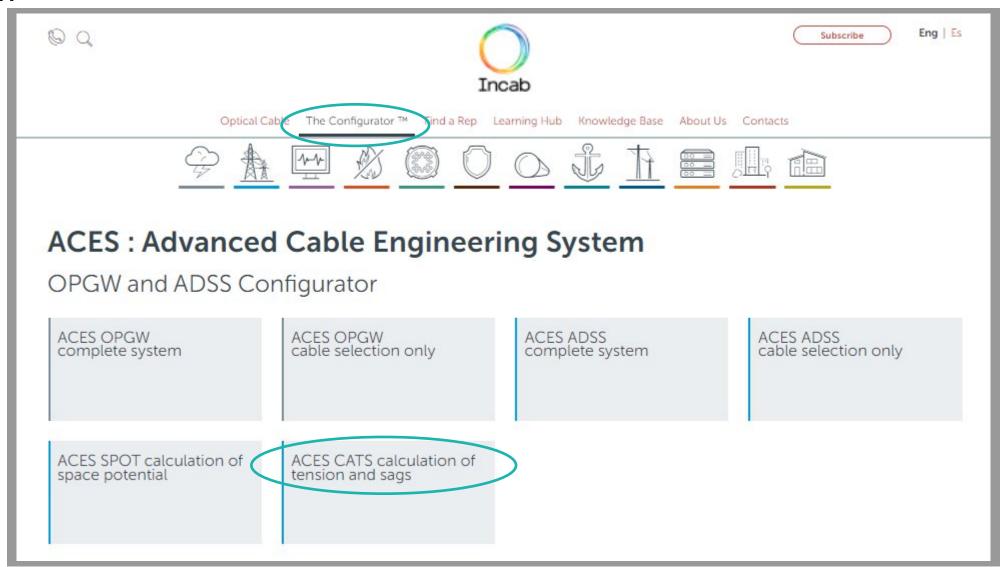
"Vert." = vertical sag to check ground clearance

GENERATING YOUR OWN DATA USING ACES CATS

- It's your data and you need it now!
- Greatly facilitates "what if" analysis
- Fast, easy, and fun (Perhaps I've been working with aerial cables too long)
- Can use for any supplier's cable!
 - You just need the basic cable data that we have discussed

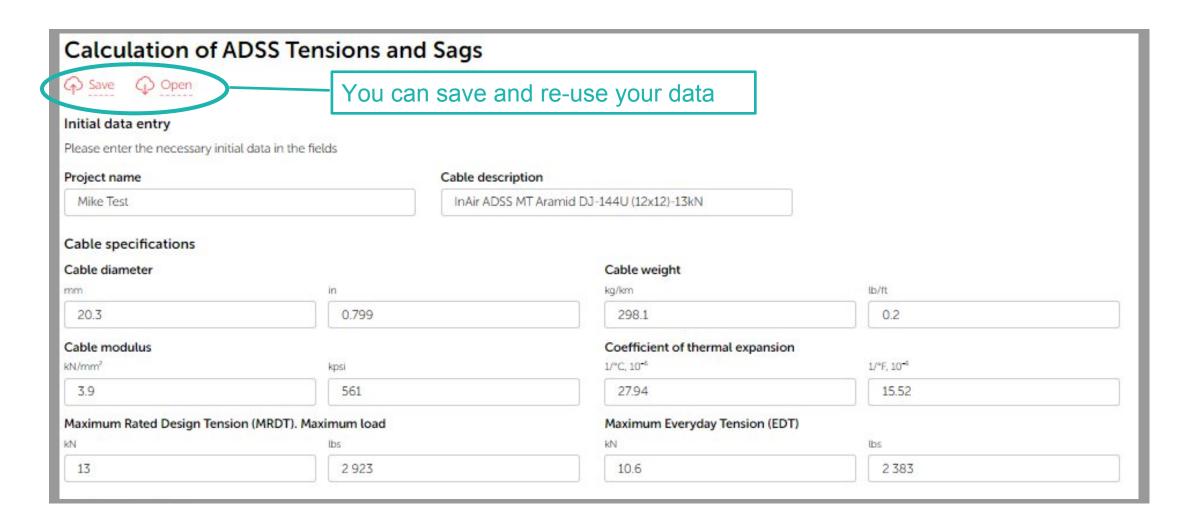
GENERATING YOUR OWN DATA USING ACES CATS

 Go to <u>www.incabamerica.com</u> and then select The Configurator™ followed by ACES CATS...



GENERATING YOUR OWN DATA USING ACES CATS

 Enter the cable data (all as we have discussed) in either customary or metric units (enter in either units...program automatically converts to the other)



GENERATING YOUR OWN DATA USING ACES CATS

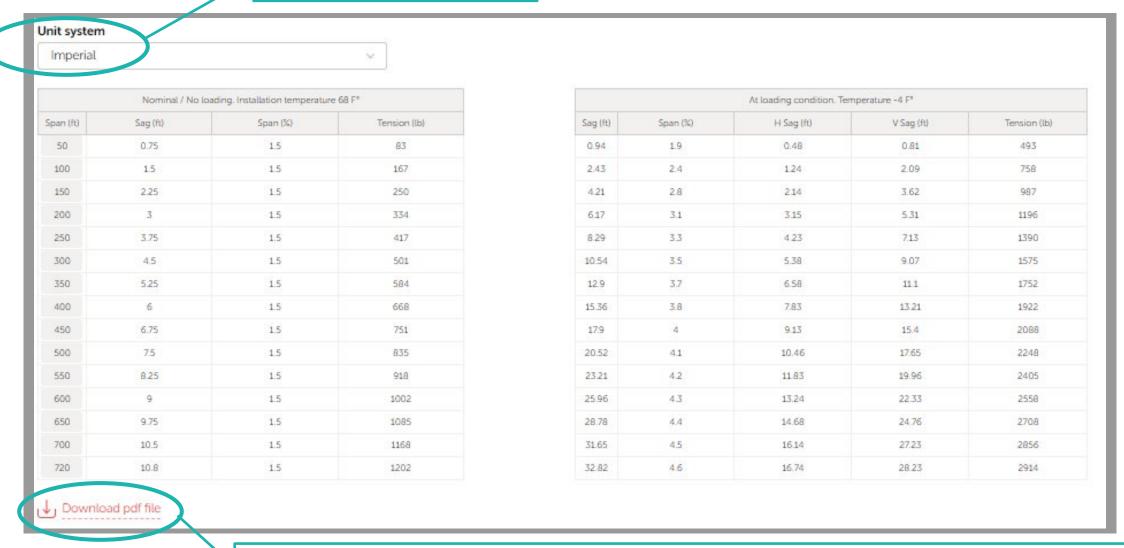
Select loading conditions or enter your own

Loading condition			
Select preset condition			
NESC Heavy		~	
Ice thickness		Wind pressure	
mm	in	N/m²	psf
12.7	0.5	191.5	4
K factor		Temperature at loa	ding condition
N/m	lbf/ft	C°	F°
4.38	0.3	-20	-4
Initial sag		Installation temper	rature
(% Span)		C*	F ^a
1.5		20	68
Calculate			

Then hit "Calculate"

GENERATING YOUR OWN DATA USING ACES CATS

Receive your data! Can change unit system



Can download as a pdf for reference or to share with colleagues, friends, or family!

CRITICALLY IMPORTANT NOTES!

All of the preceding reflects current industry practice, but strictly speaking, it is <u>not</u> correct!

- Two things are "not quite right"...
 - 1. Using only the initial value for modulus implies that ADSS is perfectly elastic with no difference between initial and final modulus, plus no creep!
 - * We know this is *not* the case
 - * Confirmed by the fact that 3 of 4 manufacturers gave different modulus values for initial, final, and 10-year/creep



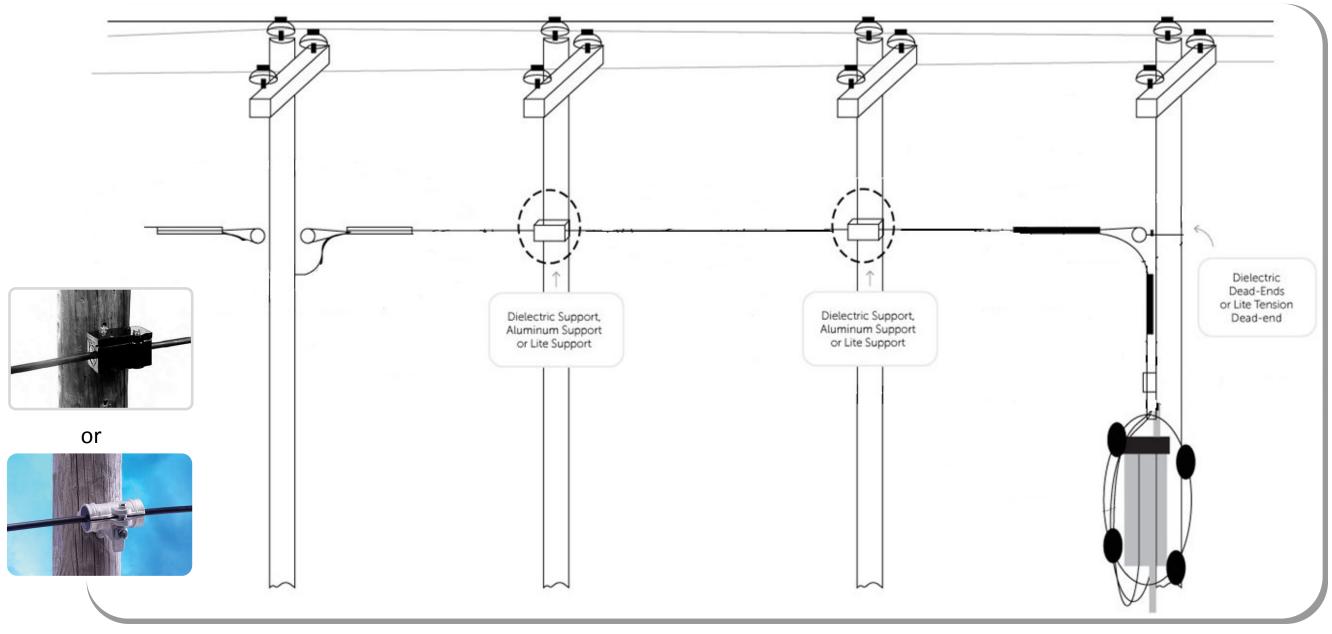
CRITICALLY IMPORTANT NOTES! (Continued)

- Spans are treated individually, as if each is double-dead-ended
 - * Only true if each span strung and clipped individually
 - "Mechanically Independent" spans (Illustrated on next slide)
 - Such as "moving reel" installation with trunnion-type support clamps
 - * More commonly, "controlled tension" stringing (tensioner and pulling line) across multiple spans is used
 - Plus, utilizing suspension clamps instead of trunnion-type supports
 - "Mechanically coupled" spans
 - Therefore, the "ruling span" concept governs the sag and tension
 - Tension equalizes across all spans with sag greatest in longer spans
 - Effectively, a weighted average (exact formula to follow soon)



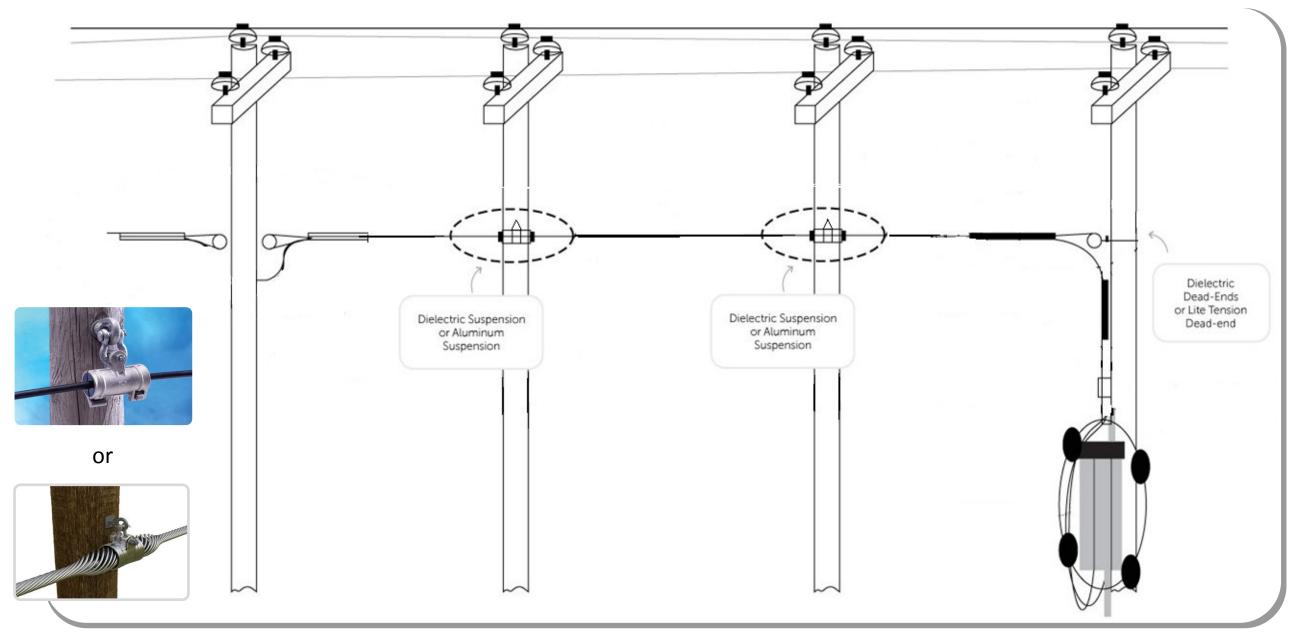
Yikes! Was everything to this point just a waste?

MECHANICALLY INDEPENDENT SPANS



Supports create fixed points at each pole, so spans are mechanically independent

MECHANICALLY COUPLED SPANS



The articulation of a suspension clamp makes the spans mechanically coupled

Sag and tension data generation UNDERSTAND THE LIMITATIONS

No! It just means you need to understand the limitations of our methodology so far!

- For "short" to "medium" spans in a distribution environment, the theoretical error is acceptable
 - * We know this is from experience, i.e. No problems in reality
 - * For ADSS, the change in sag and tension between installation (initial modulus) and final (final plus creep modulus) conditions is much lower than for metal cables (about half)
 - * Consider too sagging inaccuracies in the field
 - This "real world factor" alone likely washes out the theoretical error
- Consider our method thus far the "Simplified Sag and Tension Solution"

Sag and tension data generation methods WHEN TO USE WHAT

- OK, but now this leads to two questions:
 - 1. When is it appropriate to use the so-called Simplified Solution?
 - * First consider: What's a "short" and "medium" span?
 - Spans under 500 600 ft (≈ 150 200 m) and standard NESC loading conditions (or similar if outside the US)
 - * Distribution circuits
 - 2. What should I use when the so-called Simplified Solution is *not* appropriate?
 - - Recall that these are the third source of sag and tension data

Sag and tension data generation methods

RULING SPAN CONCEPT - DEFINED

• Mathematically: $S_R = \sqrt{\frac{\sum S^3}{\sum S}} = \sqrt{\frac{S_1^3 + S_2^3 + ... S_n^3}{S_1 + S_2 + ... S_n}}$

where:

 S_R = the theoretical ruling span

 $S_1, S_2, ... S_n$ = are the 1st, 2nd, ... n^{th} span length respectively

- In words: The square root of the sum of the spans cubed divided by the sum of the spans
 - Effectively a weighted average leaning towards the longer spans

Note: The ruling span is very easily calculated in Excel from a list of the spans. PLS-CADD can also do it for you.

Sag and tension data generation methods

RULING SPAN CONCEPT - EXAMPLE

		Span Length	
Span	Section	ft	m
1	Pole 1 - Pole 2	217	66
2	Pole 2 - Pole 3	197	60
3	Pole 3 - Pole 4	246	75
4	Pole 4 - Pole 5	213	65

$$S_R = \sqrt{(217^3 + 197^3 + 246^3 + 213^3)/(217 + 197 + 246 + 213)} = 220.4 \text{ ft}$$

 $S_R = \sqrt{(66^3 + 60^3 + 75^3 + 65^3)/(66 + 60 + 75 + 65)} = 67.2 \text{ m}$

Compare: Average span = 218.25 ft or 66.5 m

Sag and tension data generation methods

BACK TO PLS-CADD... SET-UP YOUR .WIR FILE

- Hint: It's good to know how to do this procedure and to understand what's in a .WIR file, but...
 - It's easier if you just ask for a .WIR file from the cable manufacturer
 - You can find a library of .WIR files by cable manufacturer at www.powline.com/files/cables

*Consequently, we will talk about this process very generally and very quickly

- è Editing .WIR files for ADSS is not for the faint of heart!
 - Proceed with extreme care!

BACK TO PLS-CADD - SET-UP YOUR .WIR FILE

It's best to start with a "donor" .WIR file for ADSS and edit the data as in this example:

```
aWir File template - ADSS - Notepad
                File Edit Format View Help
                TYPE='CABLE FILE' VERSION='14' UNITS='US' SOURCE='PLS-CADD Version 14.55' USER='Power Line Systems, Inc.'
                Incab ADSS DPD-E-48U (4x12)-12kN Cable designation
                Incab Cable supplier
                0 0
Required by
                DPD-E-48U (4x12)-12kN ← Cable designation, repeated
                0 10000
                0.259
                        (Cross-sectional area, in^2) ← Cross-sectional area
                0.575
                        (Diameter, in) Diameter
                        0.137
                        (Rated tensile strength (RTS) a.k.a rated breaking strength) RBS
                2698
                DATA ON THIS LINE IS NOT USED (Note: MRDT = xxxx lb) (Add a note with the "maximum allowed tensile stren
                0 12680 0 0 0
                                  (The second number is the initial modulus, using ksi value x 10)
Instead of stress-
                0 9010 0 0 0
                                  (The second number is the "10-year modulus of elasticity", using ksi value x 10)
strain coefficients.
see notes at right
                14290
                                  (The final modulus, using ksi value x 10)
                0.00058
                                  (Thermal coefficient of expansion with decimal place shifted 4 places to the left)
  Required by
                -459.67 0 0 0 0
                                  (No change)
                                                  Don't touch anything below this line ("Here be dragons!")
    program
                25 0 0 0 0 0 0 0 0 0 0 0 32 (No change after here EXCEPT for file name in line that starts with "TYPE
```

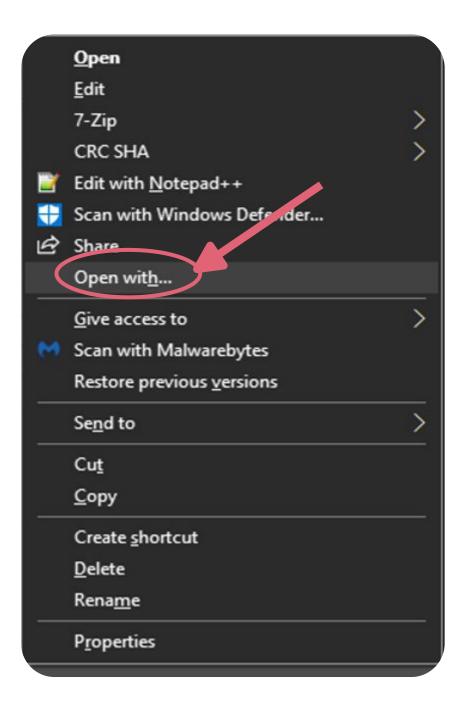
BACK TO PLS-CADD - SET-UP YOUR .WIR FILE

Don't touch anything below this line ("Here be dragons!")

```
25 0 0 0 0 0 0 0 0 0 0 0 0 32 (No change after here EXCEPT for file name in line that starts with "TYPE
           00000
           00000
             ; num pts
           0; num_pts
            1 ; cable_file_type
           0 0 32 32 0 0 0 0 0 0
Required by
  program
           020000
           010000
           255
           TYPE='Property Notes File' VERSION='1' UNITS='US' SOURCE='PLS-CADD Version 14.55' USER='Power Line Systems
           4 168
           {\rtf1\ansi\ansicpg1252\deff0\deflang1033{\fonttbl{\f0\fmodern\fprq1\fcharset0 Courier New;}}
            {\colortbl ;\red0\green0\blue0;}
            \viewkind4\uc1\pard\cf1\f0\fs20
```

Sag and tension data generation WORKING WITH .WIR FILES

- You can open a .WIR file by right-clicking on it, selecting "Open With", and then selecting "Notepad"
 - It's a text file, so Notepad works best
- After editing it, save the new .WIR file
- Then, load the new .WIR file into PLS-CADD, complete your problem file, and let the program compute the sag and tensions for you



CRITICAL FINAL STEP

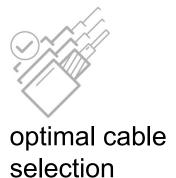
Remember MRDT? It's critical! And, ZFSM is darn important too!

- You must <u>manually</u> check in both PLS-CADD and Sag10 that tension never, ever exceeds the cable's MRDT!
 - * If it does, you risk optical problems (short or long term)!
 - * if it does, you risk a voided warranty!
- Repeat: The tension under any and all conditions must never, ever exceed the cable's MRDT!
 Important
- You should also check the Fiber Strain Margin or ZFSM as appropriate



ACES: Advanced Cable Engineering System ADSS Configurator

- Our Advanced Cable Engineering System (ACES) is a unique software tool to help engineers select the optimal ADSS design along with the associated accessories, including dead-ends, suspensions, down leads, splice enclosures, and dampers
- ACES ADSS will also help engineers and planners prepare cost estimates, generate a complete bill of materials, determine reel lengths, and plan logistics







specifications generation



design calculations

ACES was developed by Incab in partnership with Preformed Line Products, and we very much appreciate their assistance.

Start ACES



Thank

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